



# CFD Simulation of Non-Premixed NG/H<sub>2</sub> Combustion in Gas Turbines

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# Acknowledgement



Article

## Combustion Characterization in a Diffusive Gas Turbine Burner for Hydrogen-Compliant Applications

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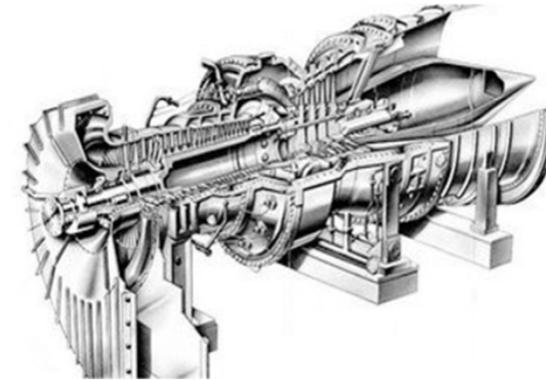
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Special thanks to:

Scott Drennan, Suresh Nambally, Gabriel Jacobson, Matteo D'Elia and Jyothish Venkataraman (Convergent Science) for their technical support

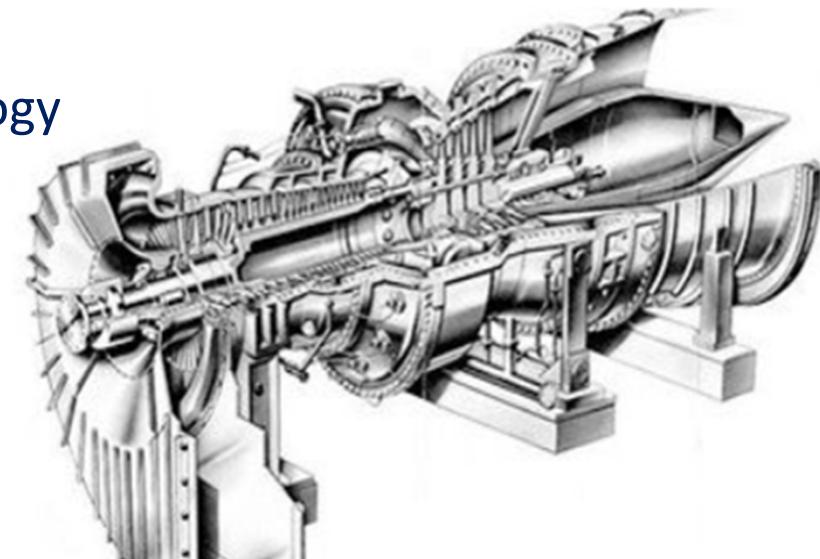
# Energy transition: the Polito and EthosEnergy strategy



- **Increasing share** of Renewable Energy Sources (RES)
- GTs: flexible and well suited for frequent starts
  - > **complementary** to the time-fluctuating RES.
  - > **enabler** for the exploitation of **long-term energy storage**

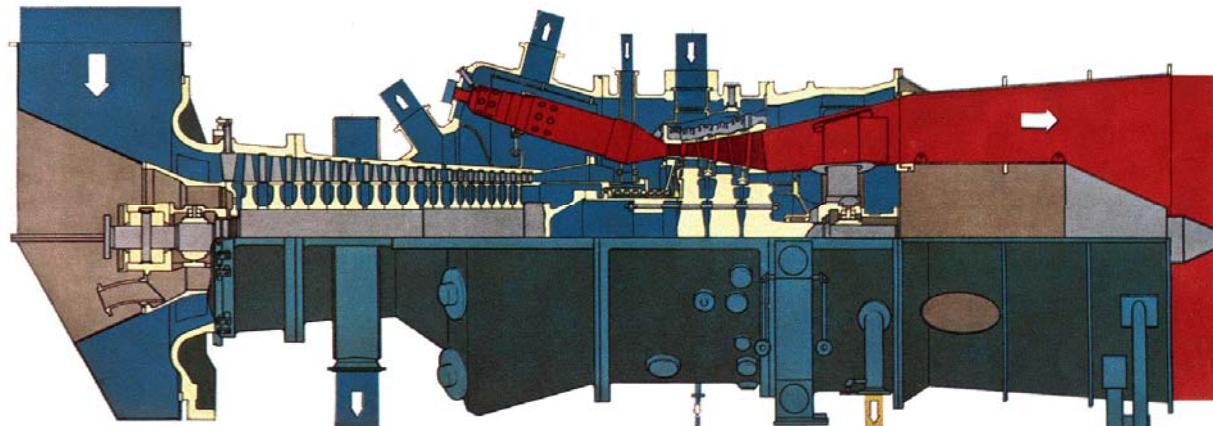
# Energy transition: the Polito and EthosEnergy strategy

- Fuel **flexibility**
  - variable blending between NG and H<sub>2</sub>
  - H<sub>2</sub> quality
- **Retrofitting** of existing turbines
  - > Lifetime extension -> economical and environmental benefits (LCA perspective)
  - > key **enabler** for the implementation of H<sub>2</sub>-GT technology
  - > small modifications of existing burners are expected
  - > increased **on-field experience** will enable further developments



Source: Hydrogen Gas Turbine Report, ETN, 2020

# Case study / Which benefit can we expect?

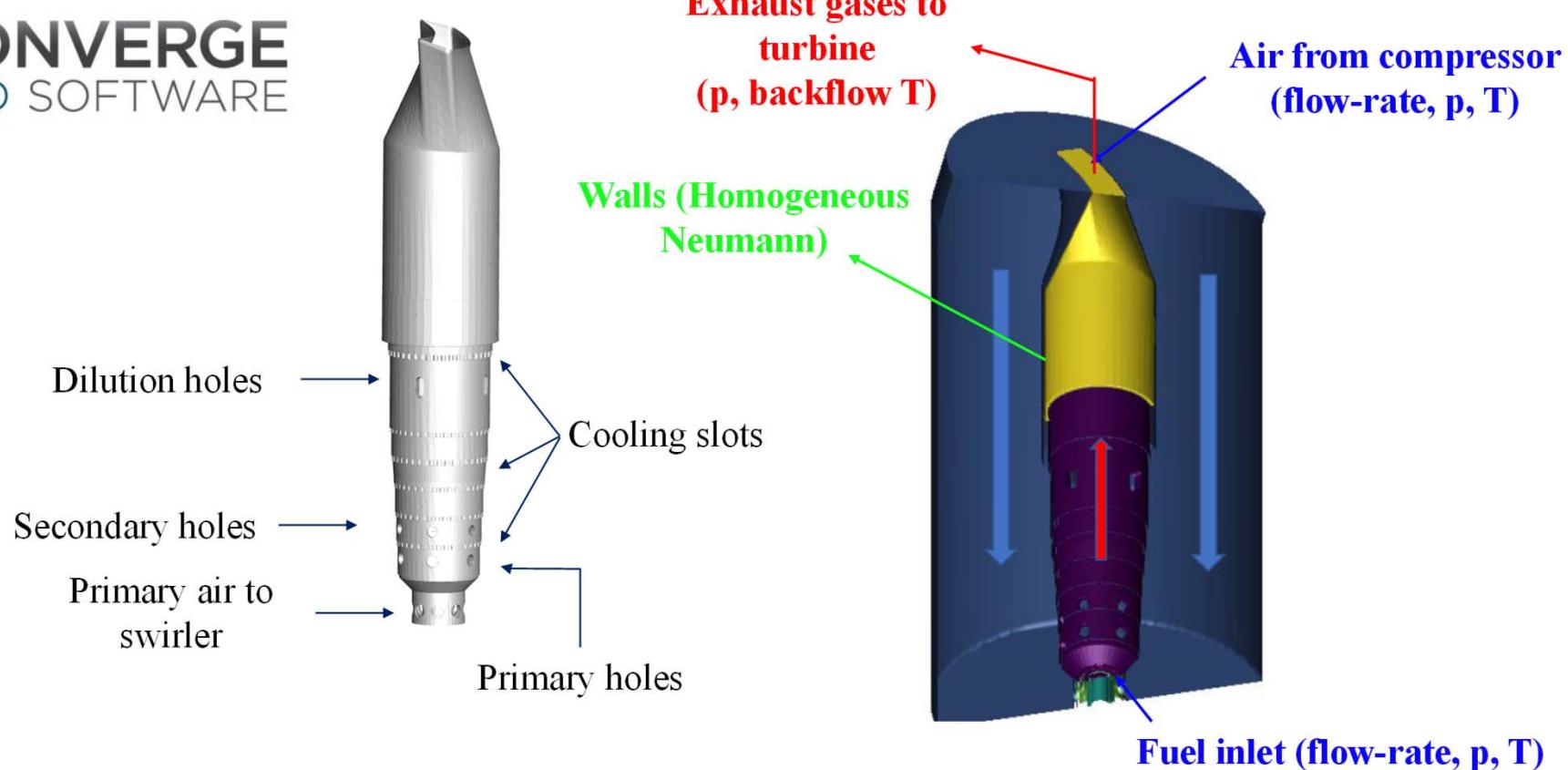


- **TG20 B7/8** turbine from EE portfolio
- Fuel rate adjusted to keep TIT constant

	NG	HCNG-15%	HCNG-25%	HCNG-50%
H/C ratio	3,3	3,6	3,9	5,9
LHV [MJ/kg]	41,6	43,3	44,7	50,3
Fuel rate [%]	100	96	93	83
<b>CO<sub>2</sub> mass emissions [%]</b>	<b>100</b>	<b>92</b>	<b>88</b>	<b>72</b>

# Case geometry and BCs

**CONVERGE**  
CFD SOFTWARE





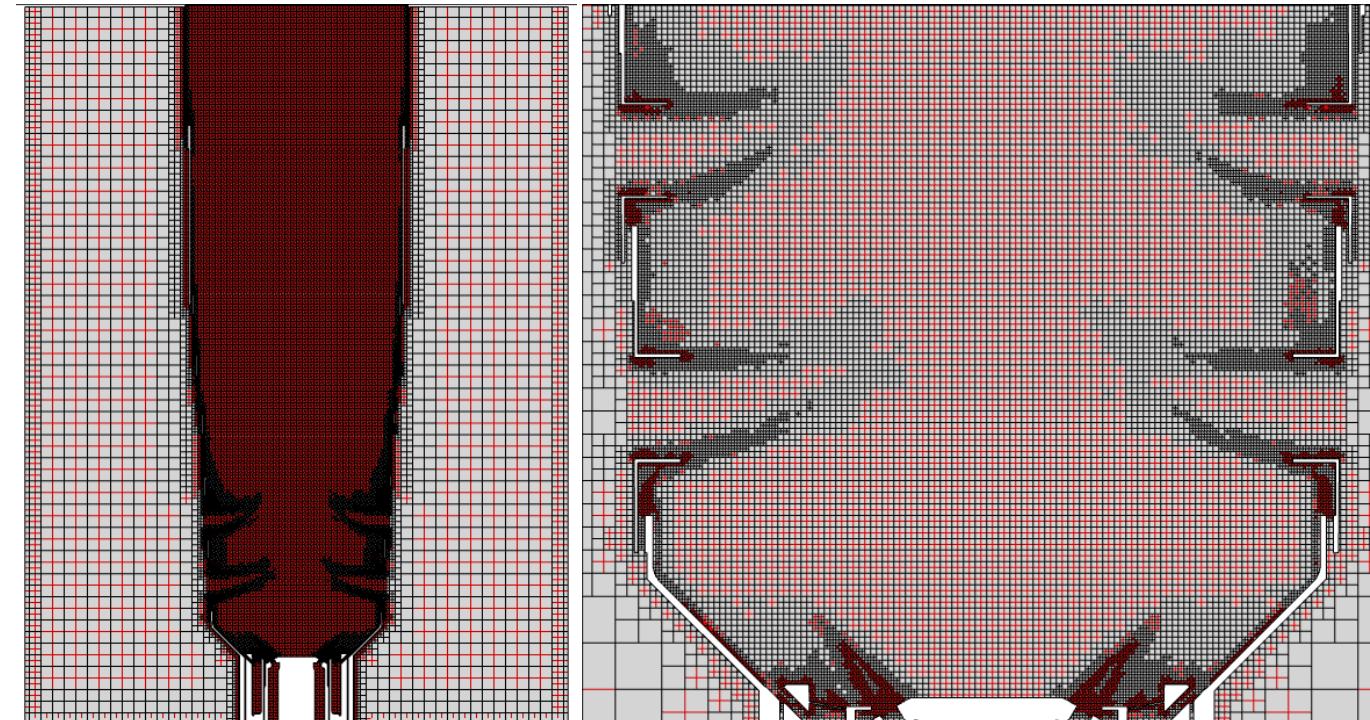
## Case setup



Solver	Steady-state, PISO
Flux scheme	2 <sup>nd</sup> order upwind (MUSCL)
Turbulence Modeling	k- $\varepsilon$ RNG (RANS)
Combustion Modeling	FGM 1D diffusive
Reaction Mechanism	GRI-Mech 3.0
Initialization	Mapping from a 1st order solution
Base grid size	20 mm
Fixed embedding in casing and TP	5 mm
Miminum size (FE)	0,156 mm (injector holes)
Minimum size (AMR)	1,25 mm (Temperature, entire domain)



# Grid independence analysis



**Red** lines

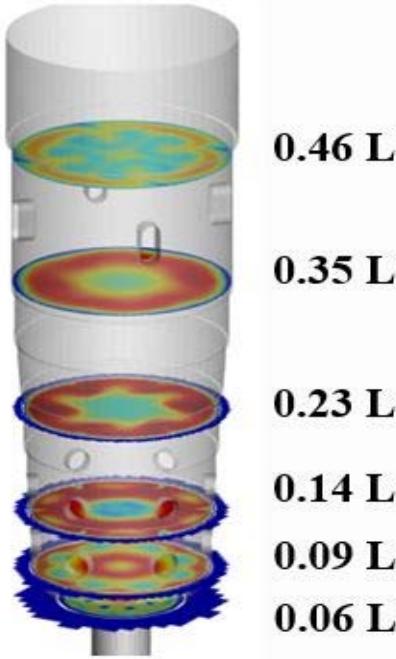
indicate that the grid size of the **refined** mesh is lower.

Average number of cells in the liner region (TP excluded):

5,5 M (**base**)

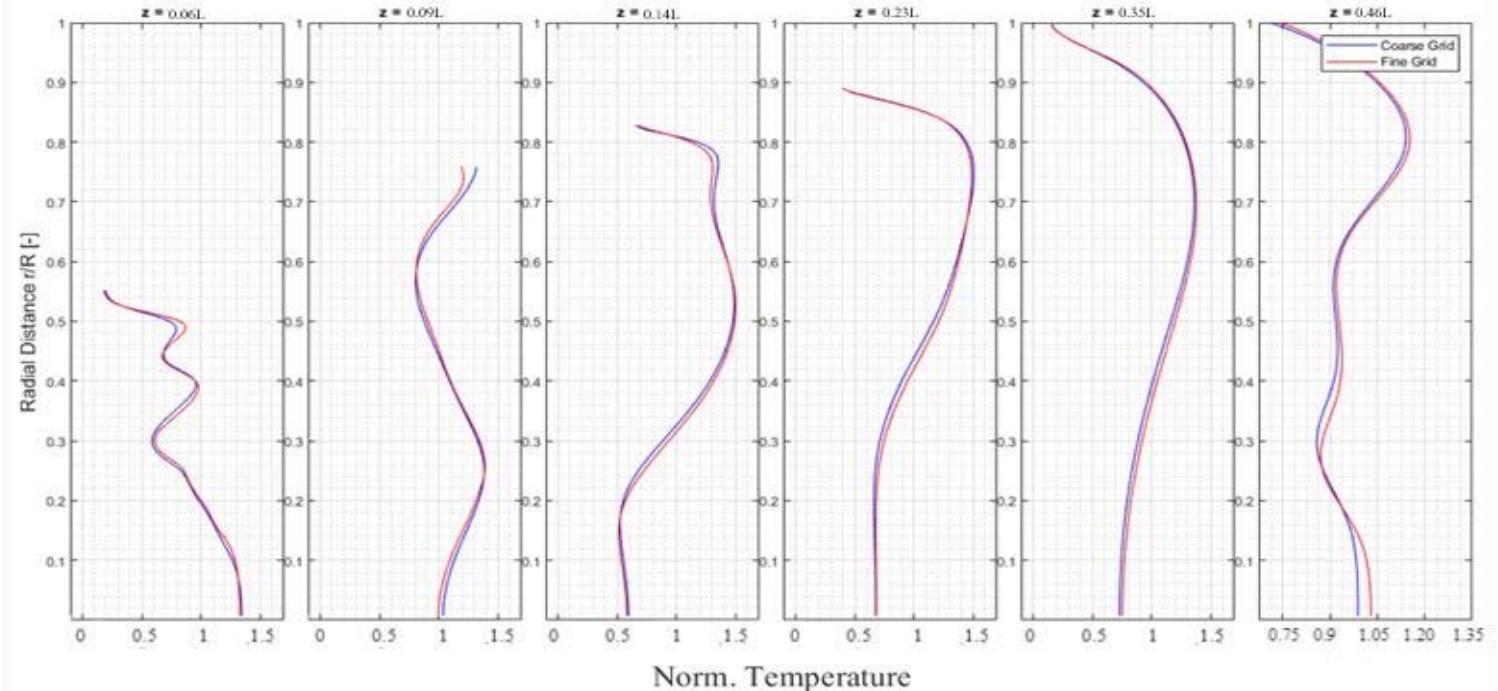
20 M (**refined**)

# Grid independence analysis



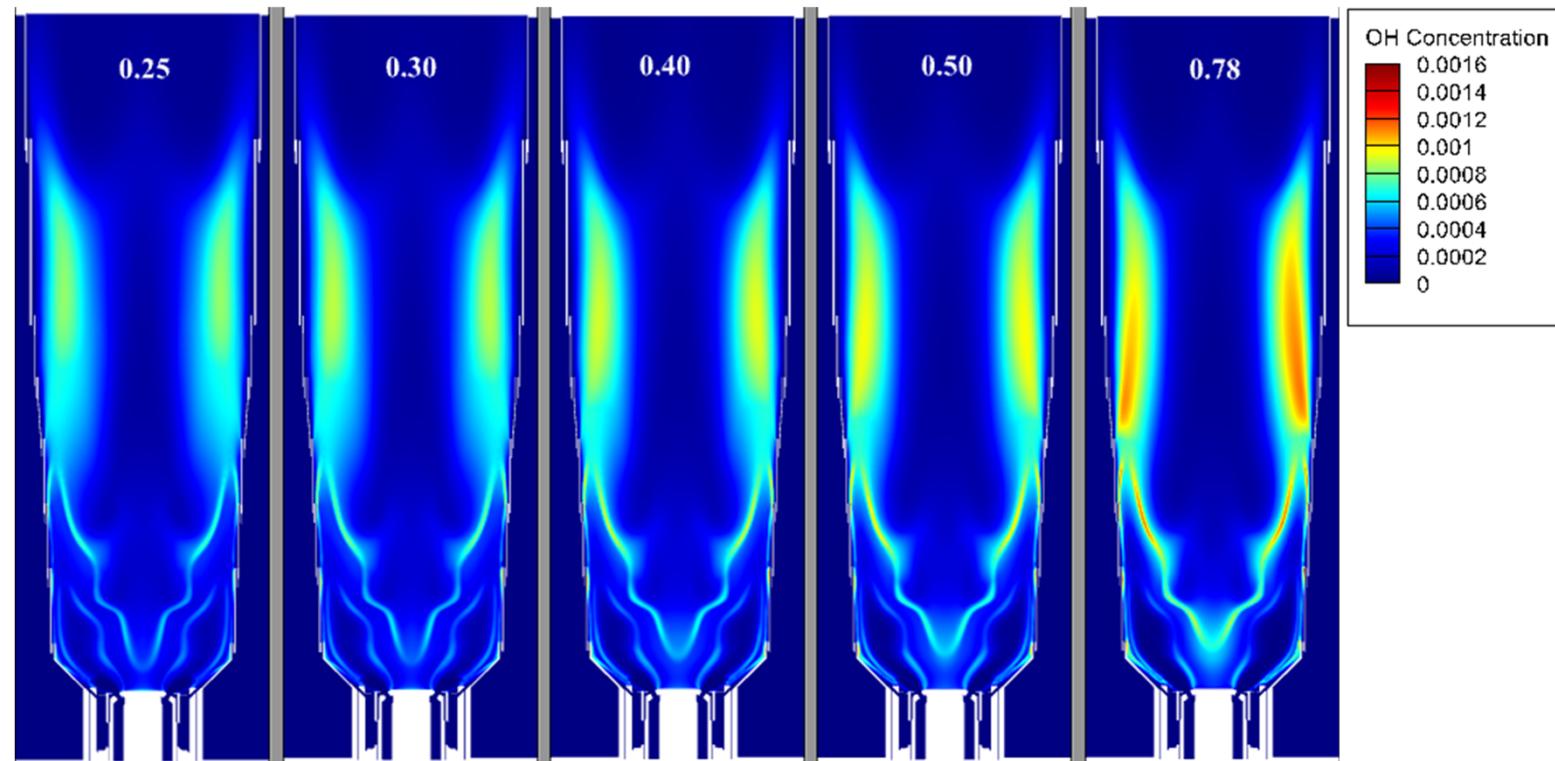
**L = Combustor Length**

N.B. Contour data are from fine grid.



# Schmidt number sensitivity analysis (1)

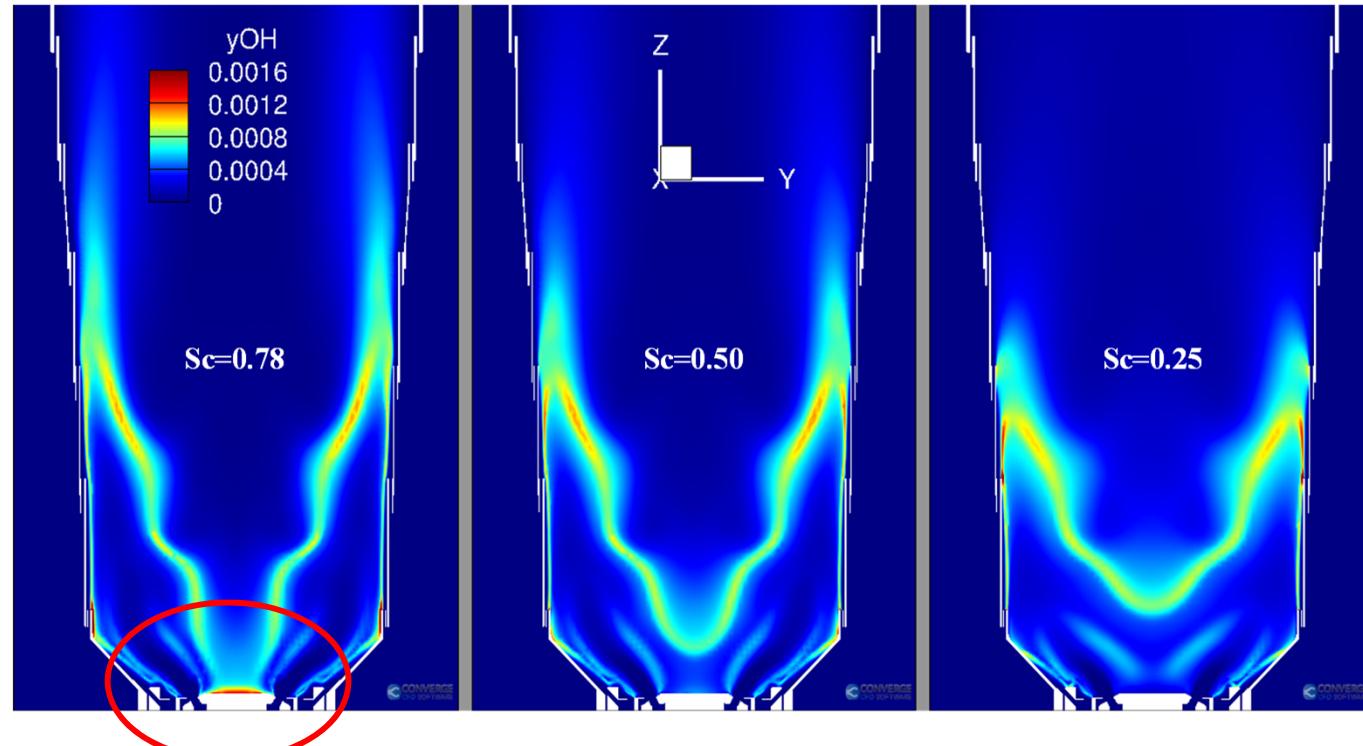
Base load condition with NG



# Schmidt number sensitivity analysis (2)

70% load case with NG

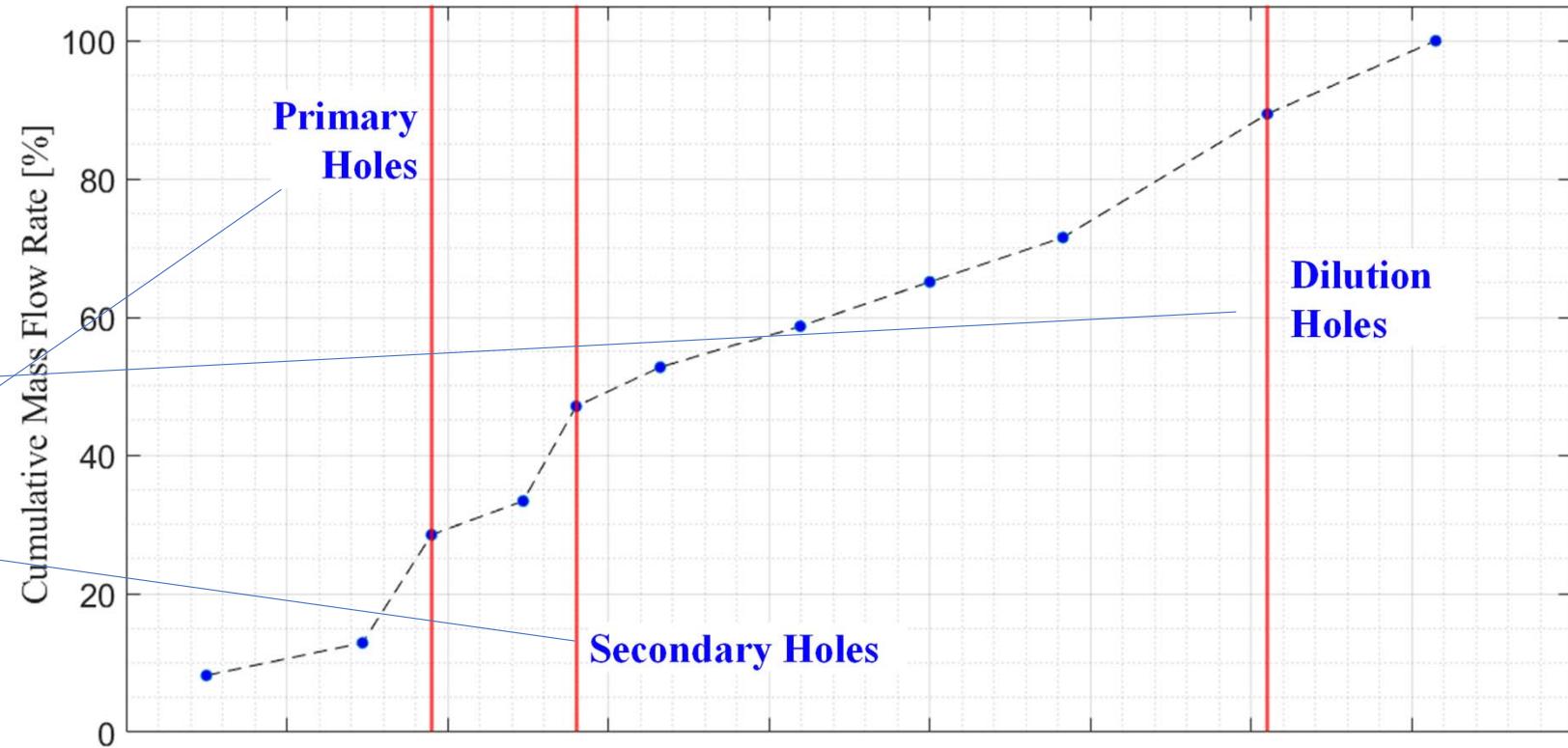
- Same **air** mass-flow rate as base load
- Lower **fuel** rate



No flame lift-off

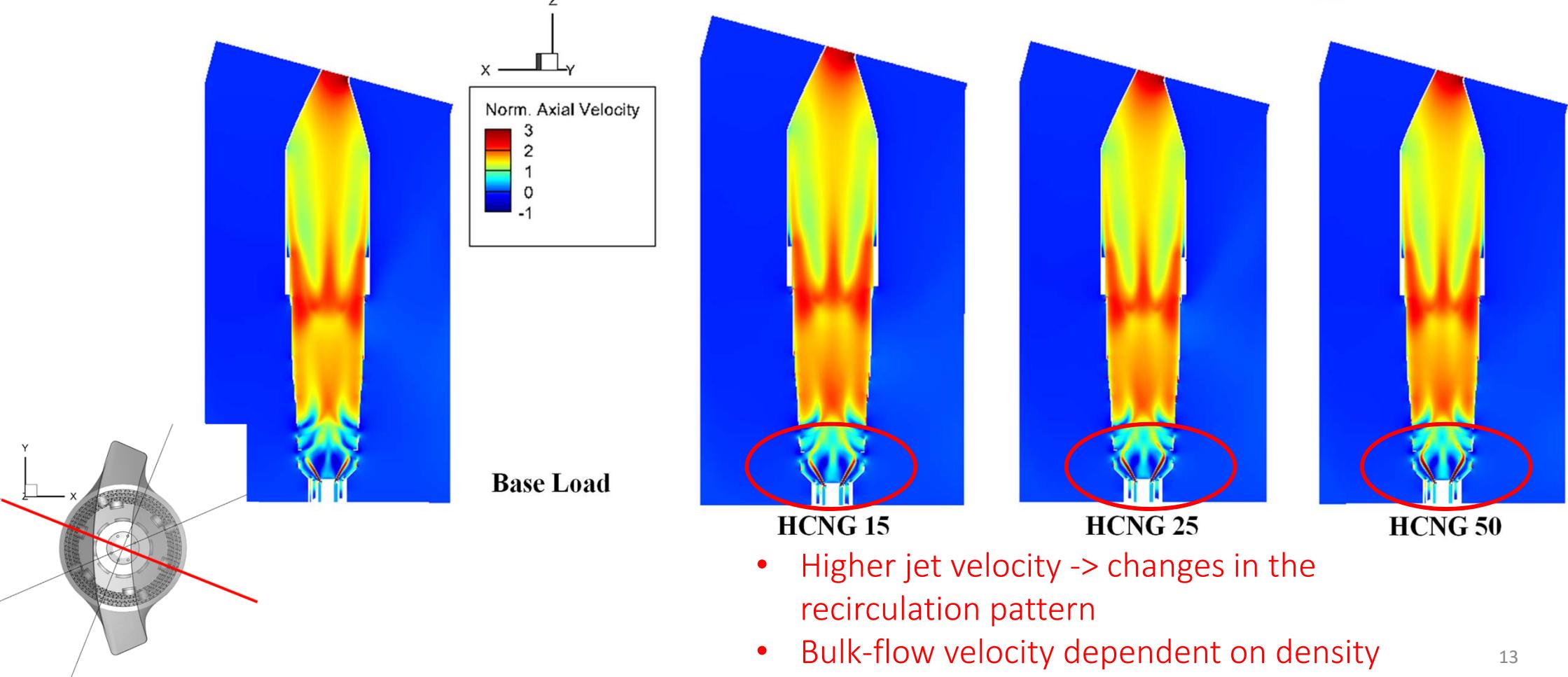
# Results

## Total mass-flow rate vs. axial position



# Results

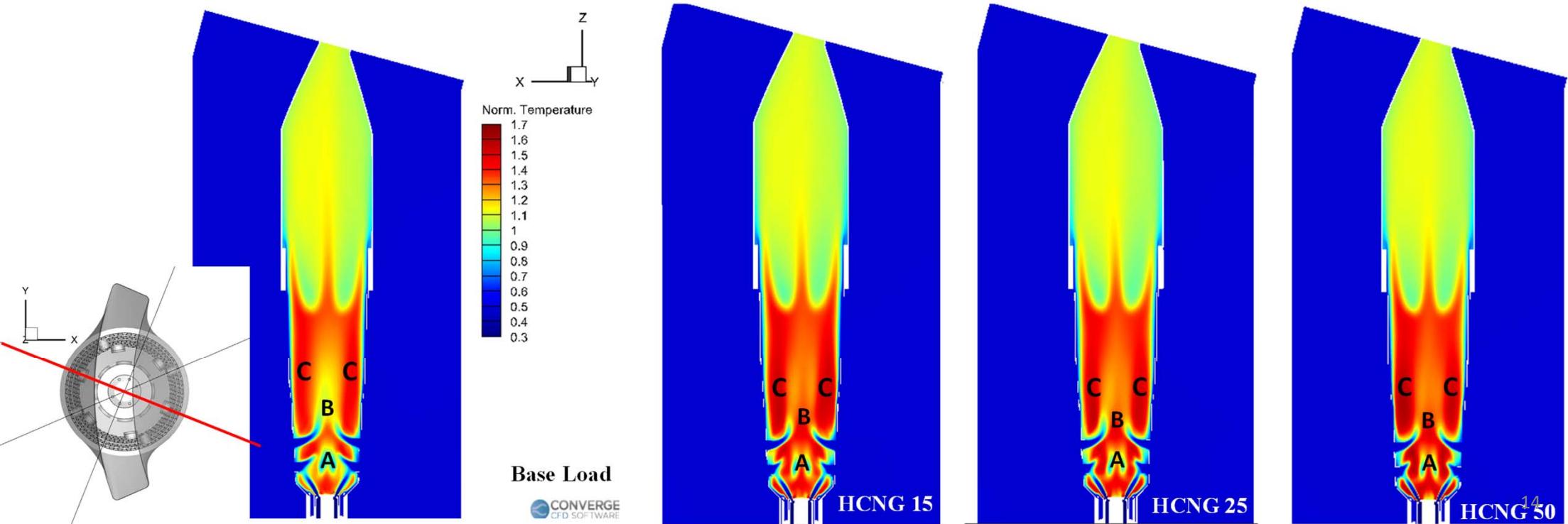
Axial velocity contours in a plane through primary and secondary holes



# Results

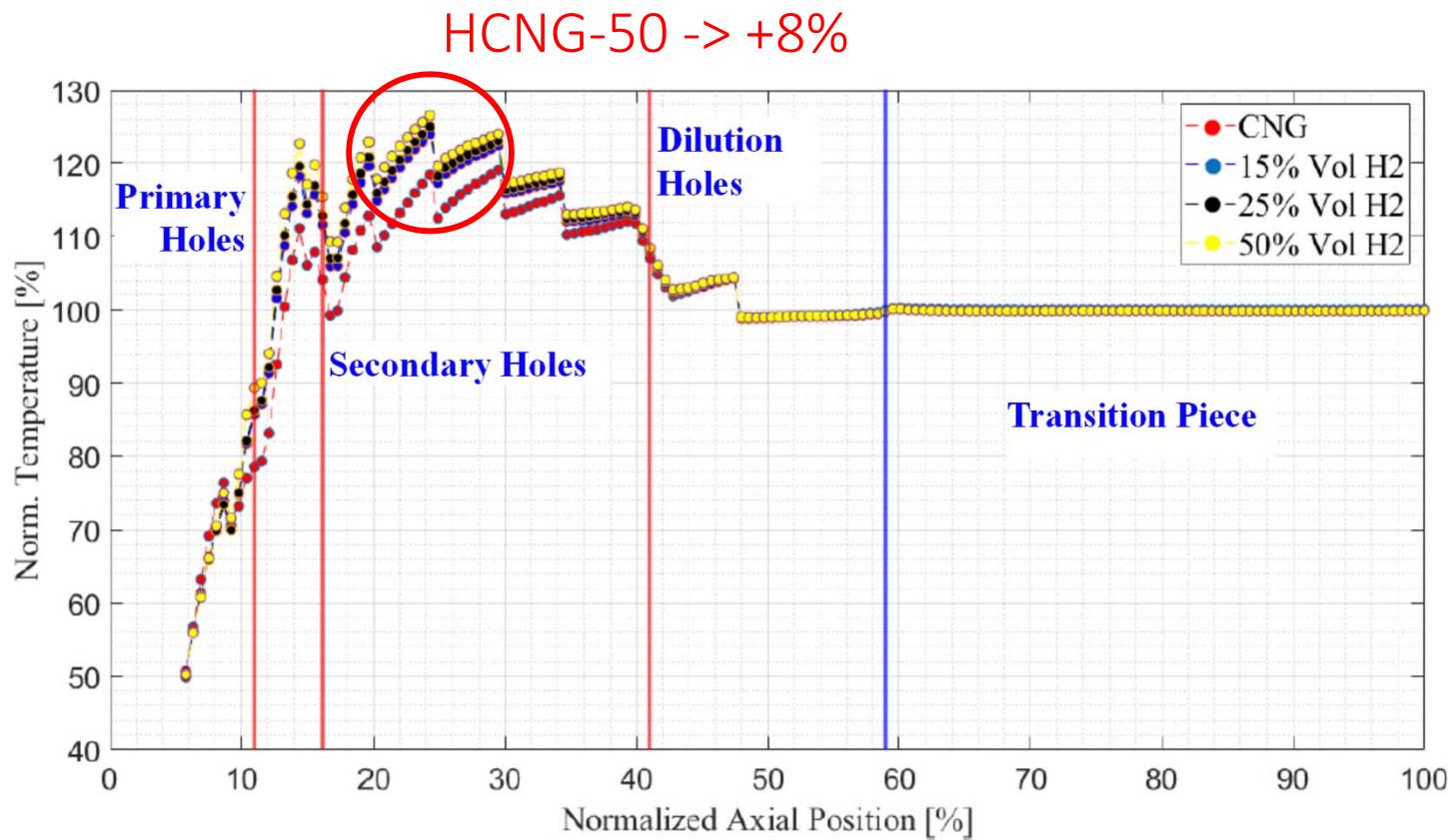
Temperature contours in a plane through primary and secondary holes

- A: recirculation
- B: 'central' hot zone
- C: 'peripheral' hot zone

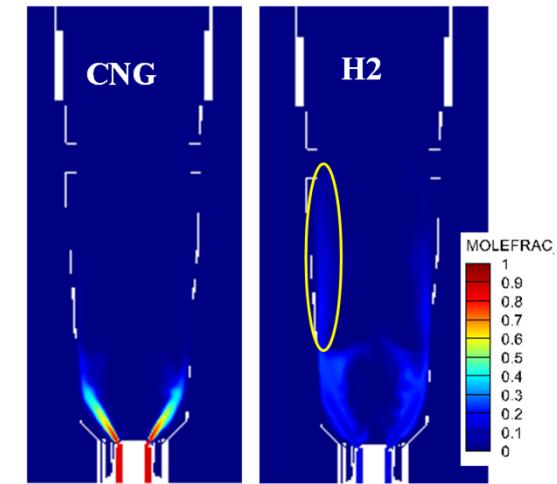


# Results

Average temperature vs axial position



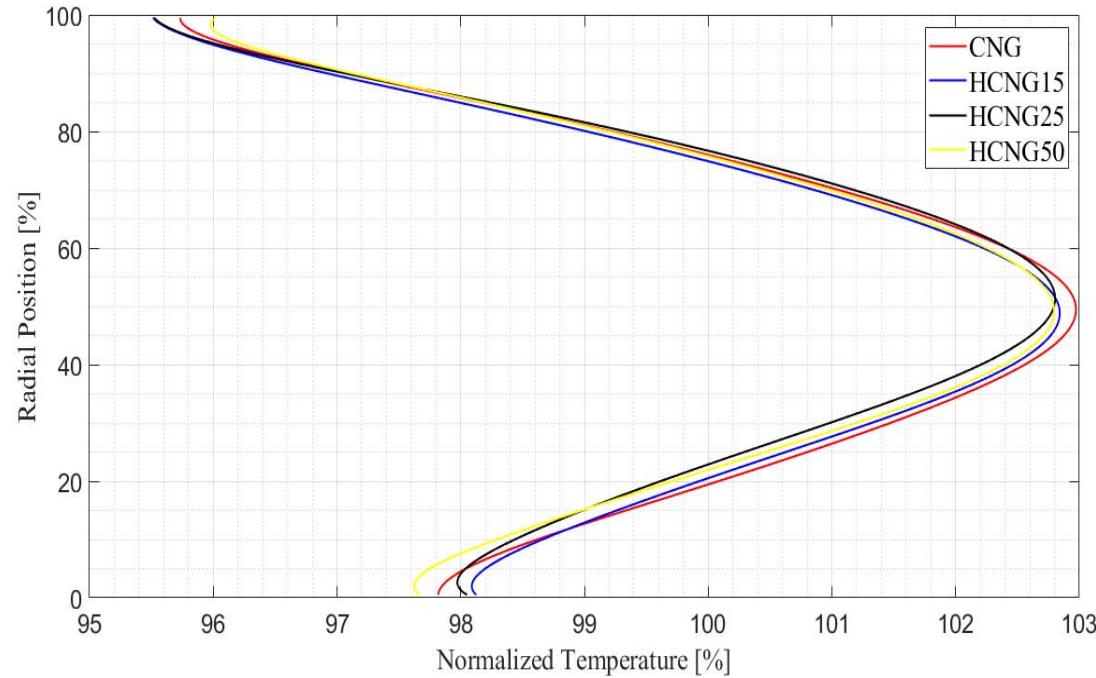
Nonlinear behavior:  
longer path for H<sub>2</sub>



- Hydrogen:
- $2,4 \times (\text{LHV})_{\text{NG}}$
  - $2 \times (\text{A/F})_{\text{st,NG}}$

# Results

## Radial temperature profile

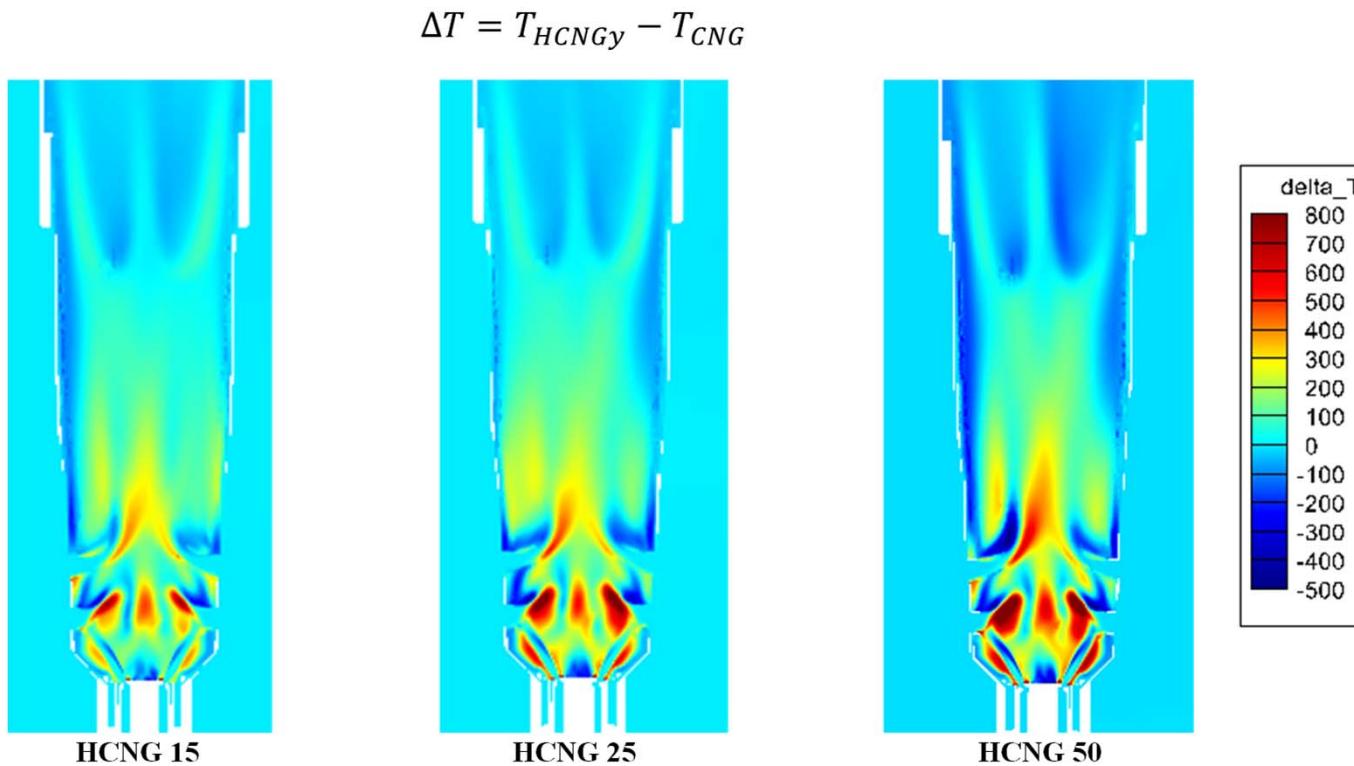


No significant changes if H<sub>2</sub> is added to NG (being TIT fixed)

-> Constant pattern factor

# Results

## 'Differential' temperature maps



Maximum temperature increase as high as **800 K**

- NOx ?
- Mechanical stresses ?

(Currently under investigation)



## Conclusion (1)



- Model development and application successful
- The combustion process in a non-premixed gas turbine burner, which is originally designed for CNG fueling, was characterized for different hydrogen blends.
- The analysis was aimed at finally retrofitting a 40 MW heavy-duty gas turbine.



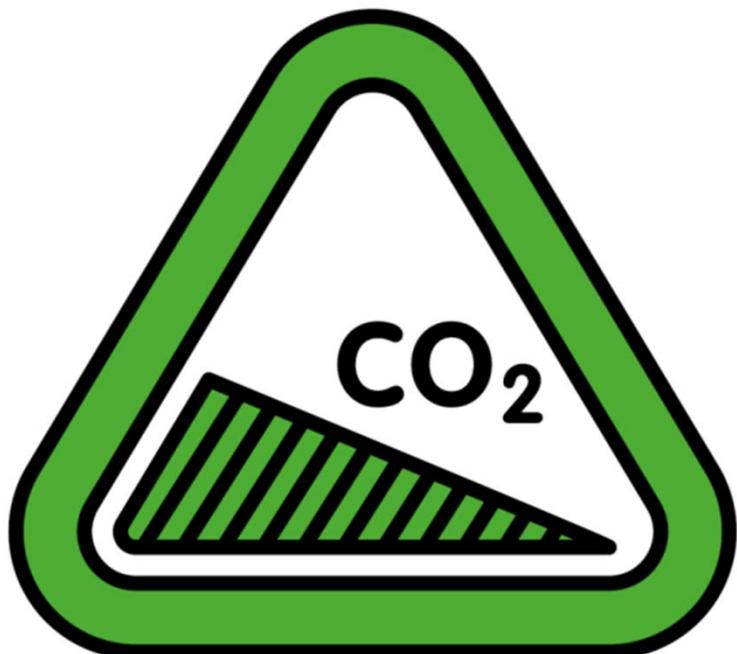
## Conclusion (2)



- A local increase in the temperature up to 800 K was obtained, as a combination of the LHV,  $(A/F)_{st}$ , and increased diffusivity effects.
- Further work is required before the effective retrofitting can be realized :
  - Careful consideration of the NOx compensation strategies (water injection and/or turbulence optimization)
  - Injector and swirler thermal stresses analysis
  - Assessment of possible design changes (taking also fuel flexibility into account)



Thank you for your  
attention!



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